

Aerodynamic Optimization of a Two-Dimensional Two-Element High Lift Airfoil with a Smart Droop Nose Device

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Motivation

Year 2001:
European Aeronautics
A vision for 2020

Advisory Council for
Aeronautics Research
in Europe (ACARE)

„A reduction in
perceived noise
to one half of
average levels“

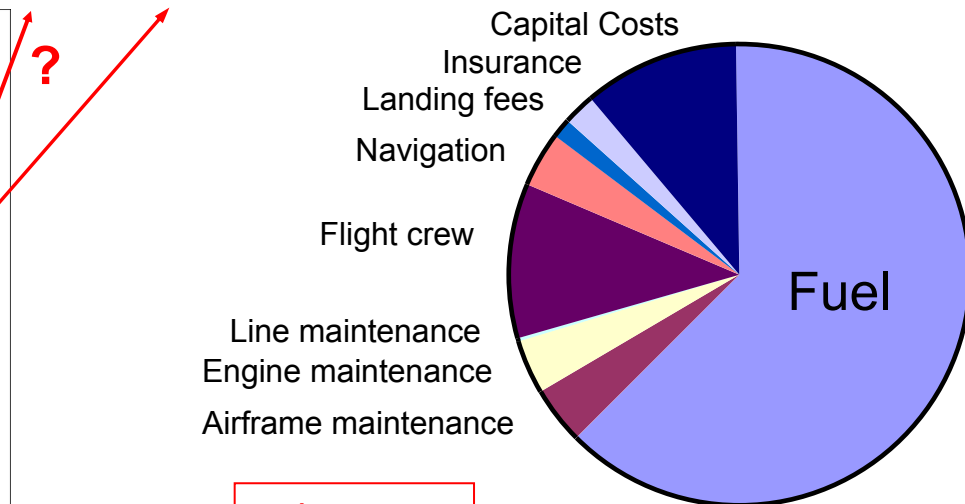
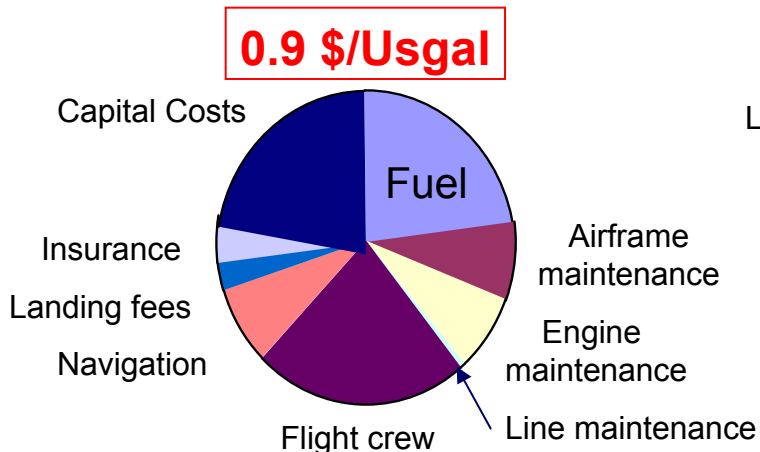
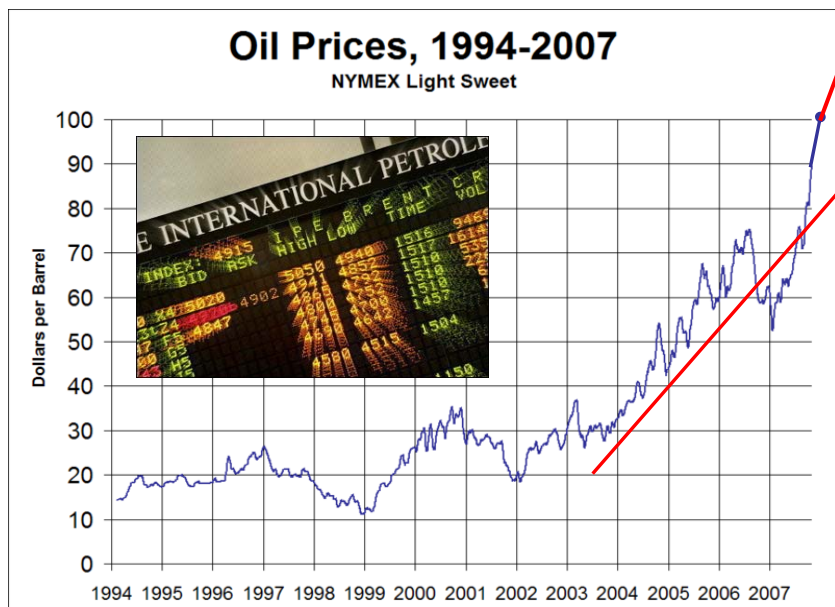
„A 50% cut in CO₂ emissions
per passenger kilometre
(which means a **50% cut in
fuel consumption** in the new
aircraft of 2020) and an 80 %
cut in nitrogen oxide
emissions“



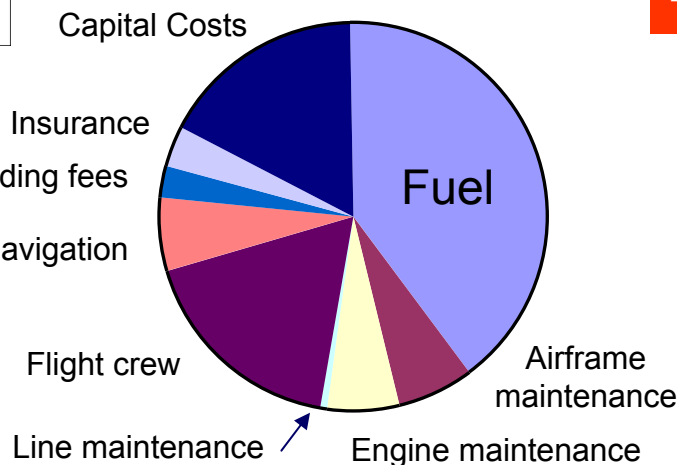
L/R DOC Sensitivity for Fuel Price Development

Oil price hit 100 \$/Barrel for the first time on Jan 3rd 2008 !

5 \$/USgal



2 \$/USgal



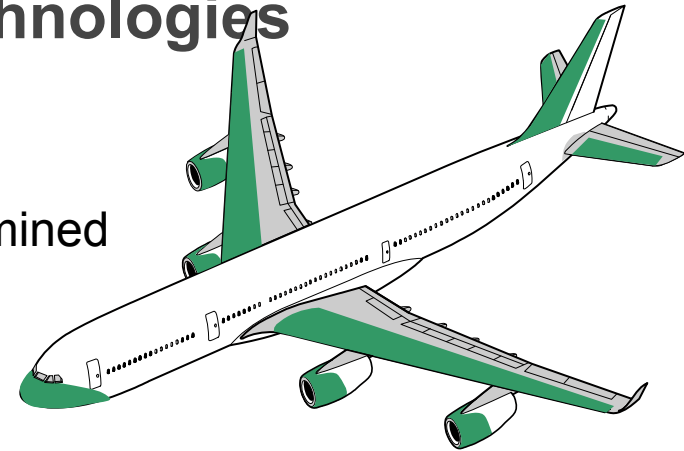
+104 %

+28 %

based on A330-200 type a/c with 1990 technology

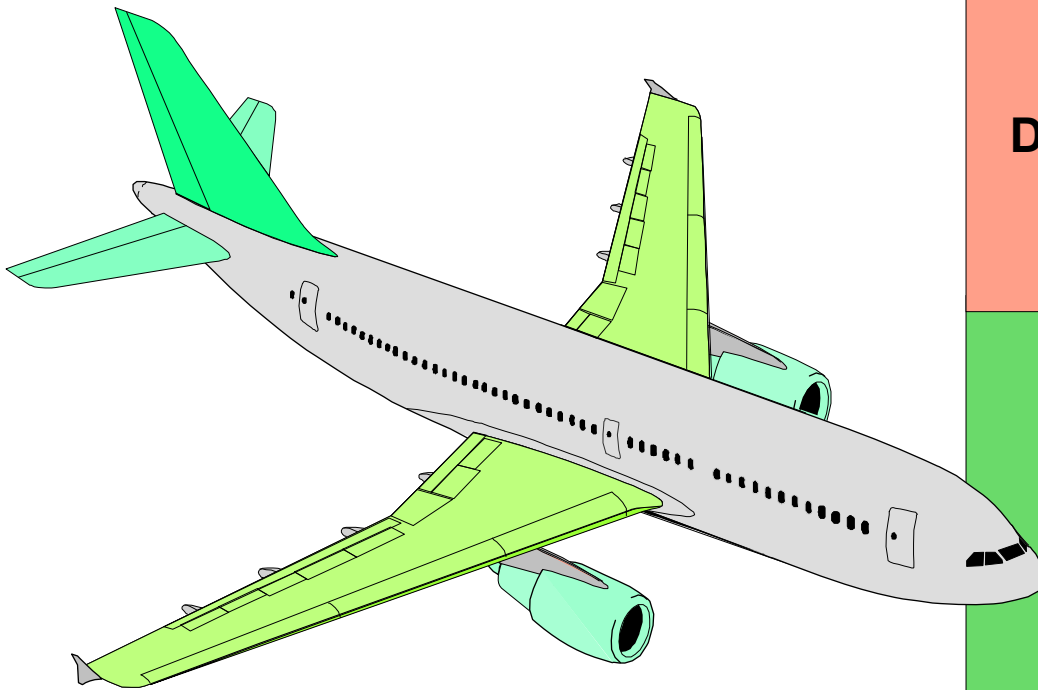
Motivation – Drag Reduction Technologies

- Many technologies have been and are examined
 - Laminar flow, distributed roughness, bumps, dimples, plasma, synthetic jets, ...
- Laminar flow technology is the only single technology with the potential to reduce drag and hence fuel consumption considerably.
- Snowballing effects add to the effect of pure drag reduction and pay off in lower mass.
- NLF or HLF with simplified suction systems are feasible.
- Operational aspects (loss of laminarity) can be handled similar to ETOPS.
- The potential of laminar flow technology is big:
 - 15 - 20% overall aircraft drag reduction feasible

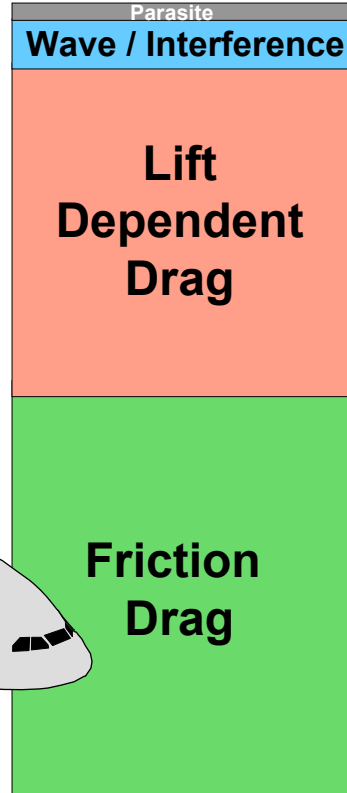


Drag Reduction – Where ?

Drag distribution on aircraft level



Total Drag

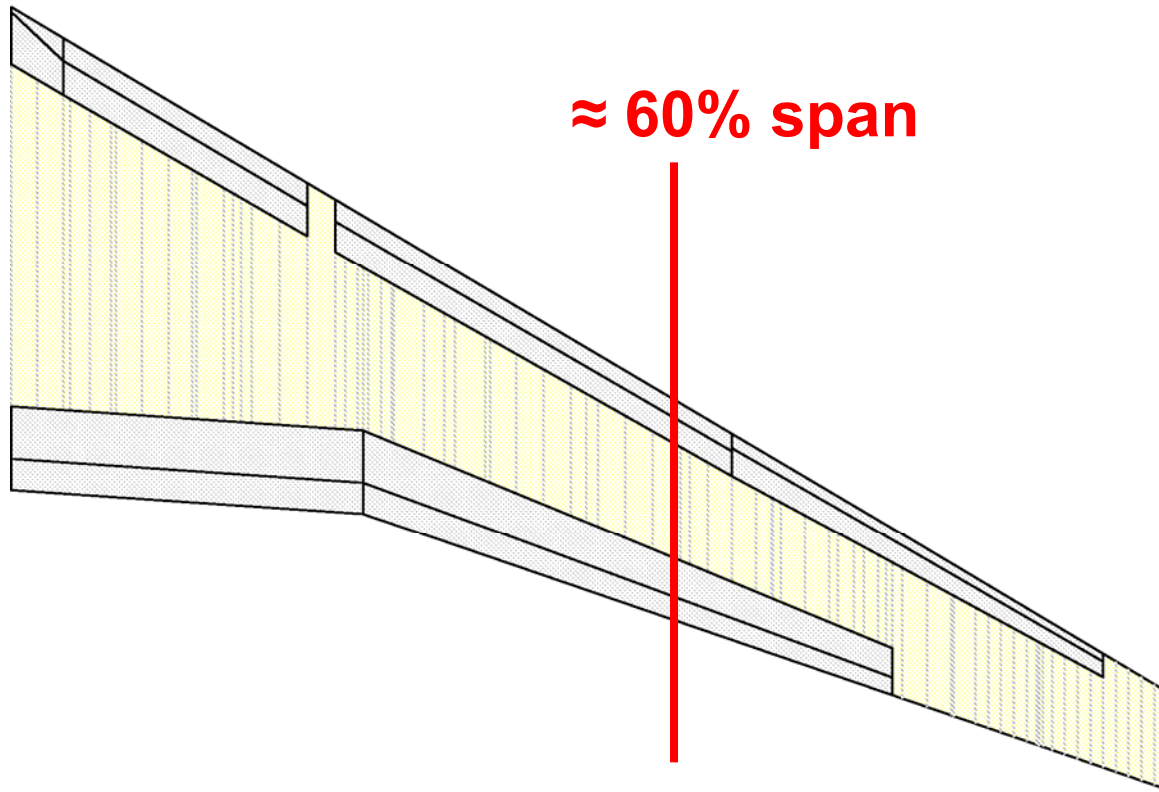


Friction Drag



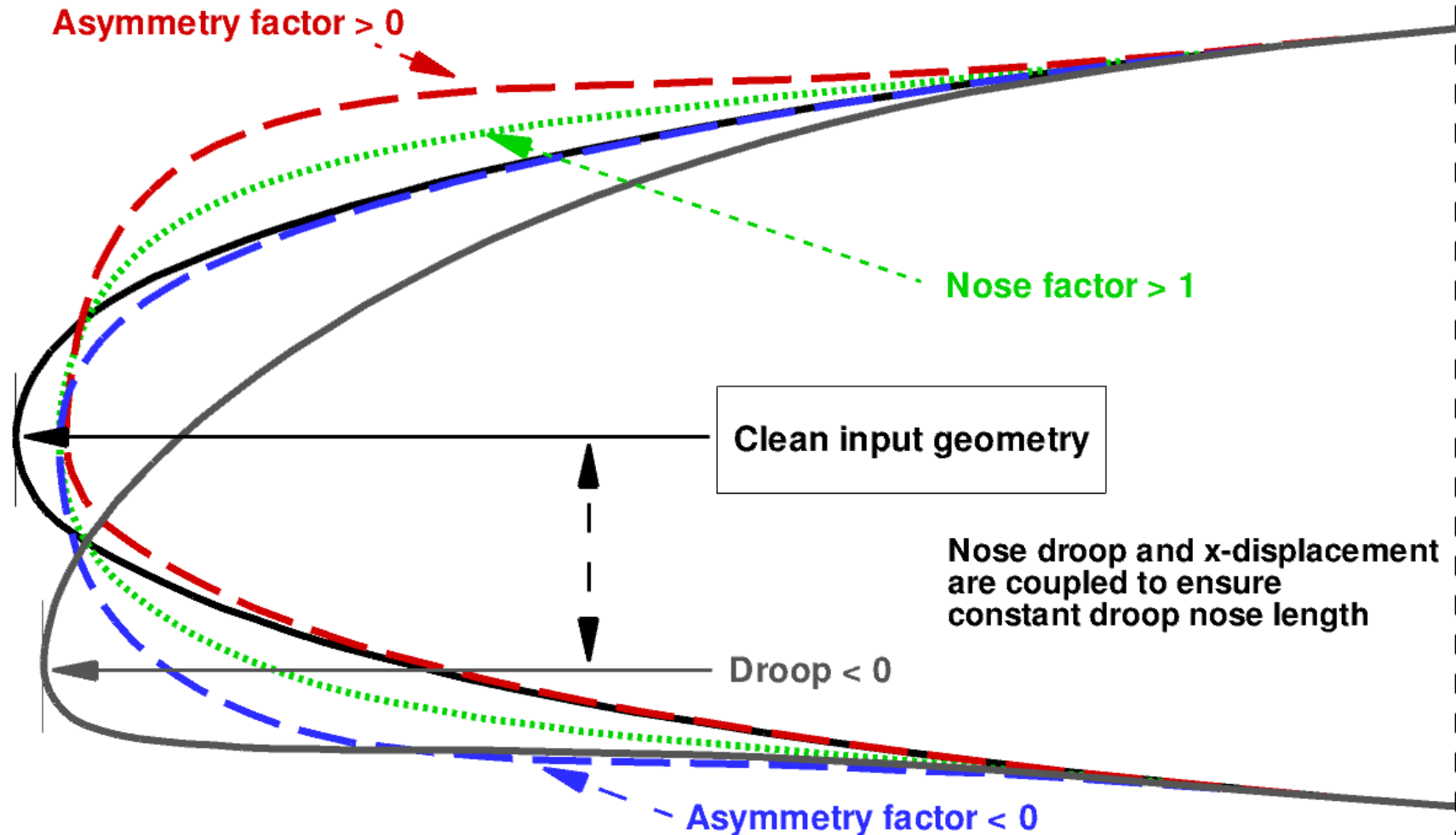
> **Wing** offers (besides fuselage) highest potential for friction drag reduction

Model



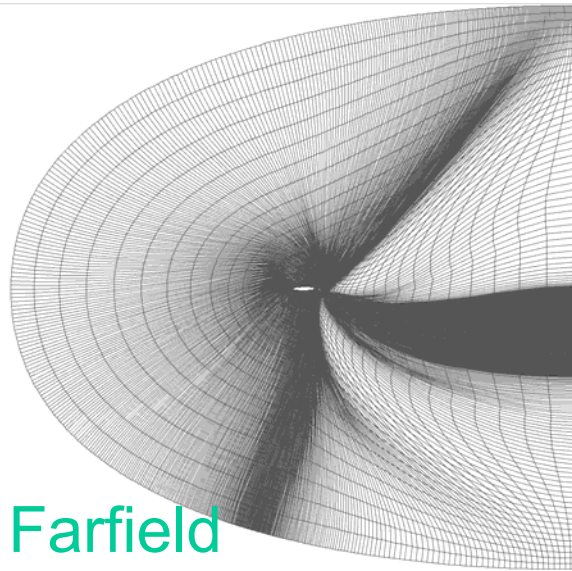
Flügel Neuer Generation = New Generation Wing

Parameterization

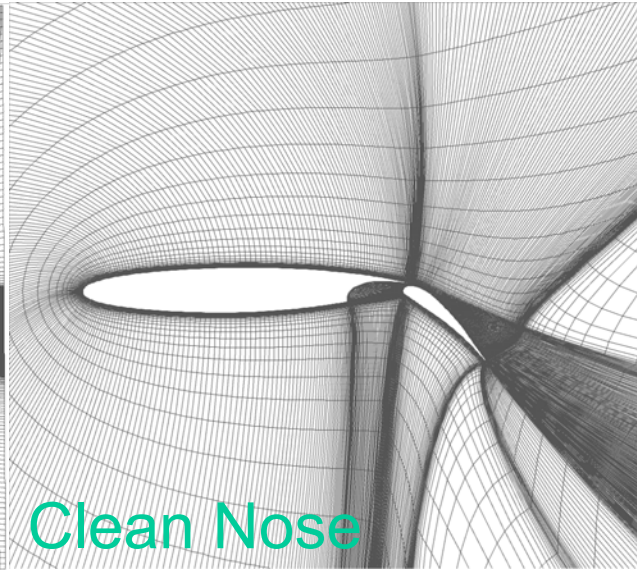


Numerical Setup - Mesh

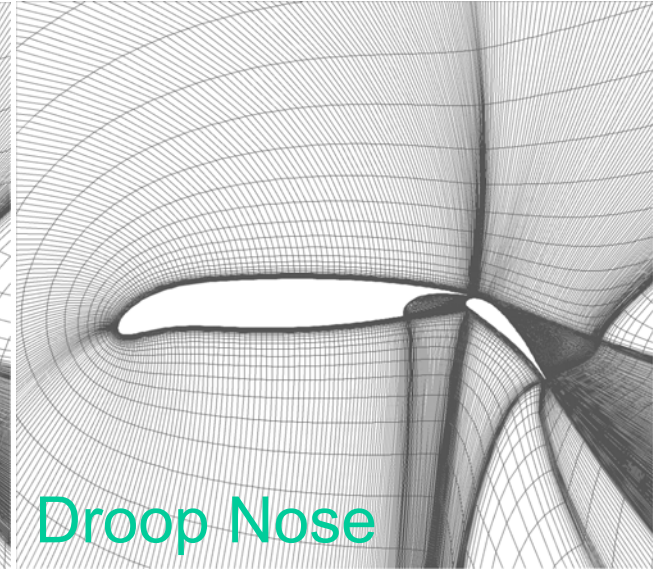
- Structured grid generator MegaCads
- Parametric grid setup allows deformation of mesh during optimization (clean nose -> droop nose)
- 65,200 nodes in 16 blocks



Farfield



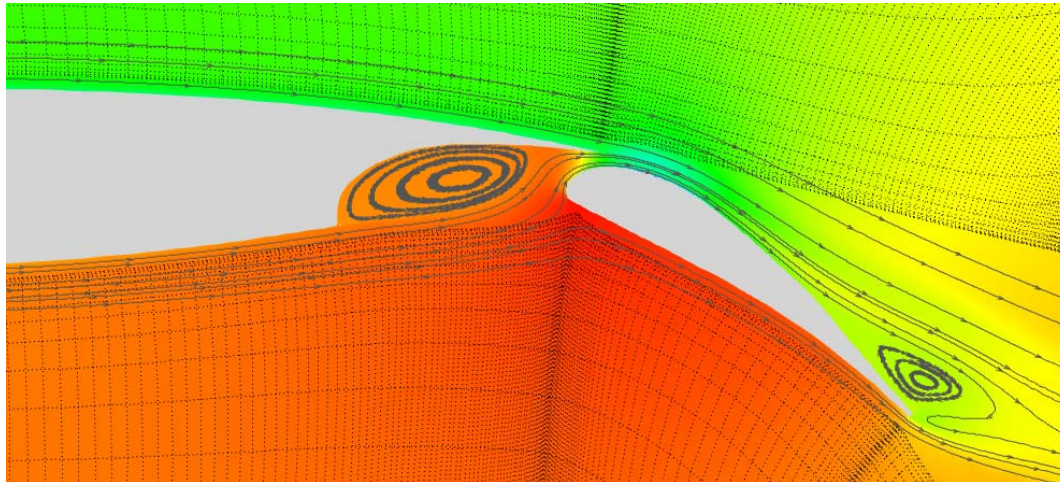
Clean Nose



Droop Nose

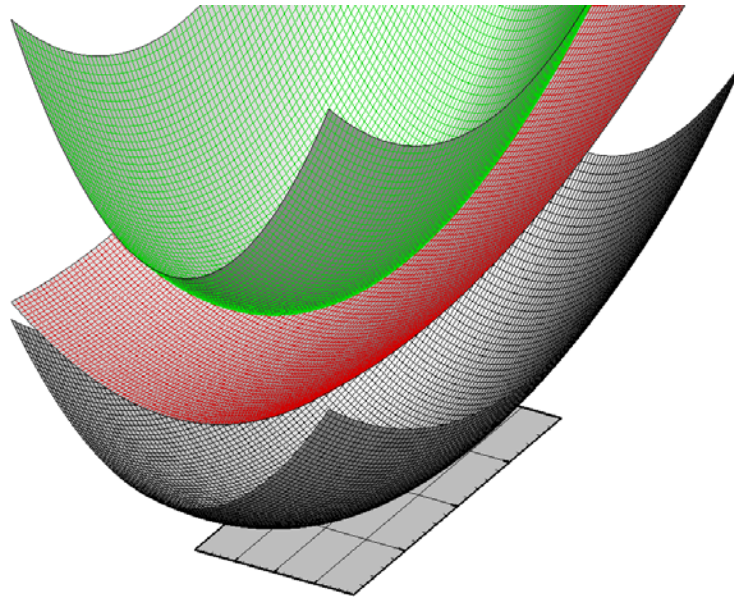
Numerical Setup – Flow Solver

- Block Structured Flow Solver DLR FLOWer
- SAE – Spalart Allmaras Turbulence model with Edwards Modification
- Convergence Acceleration (3w Multigrid Cycle, implicit residual smoothing)
- CFL number 9.5
- Automatic $C_{L,Max}$ routine for maximum lift calculations



Numerical Setup – Optimization Framework

- CHAeOPS is a DLR in-house optimization package
- Includes several optimization strategies (deterministic methods, gradient-based methods, stochastic models)
- Here: SUBPLEX (Rowan 1990)



Objective Function

Landing

$$f_{obj, L} = -C_{L, Max} - C_{L, \alpha = 0}$$

Maximum Lift
Performance

Lift Performance at
lower AoA

Take Off

$$f_{obj, TO} = C_D|_{1.13V_S} + C_D|_{1.5V_S}$$

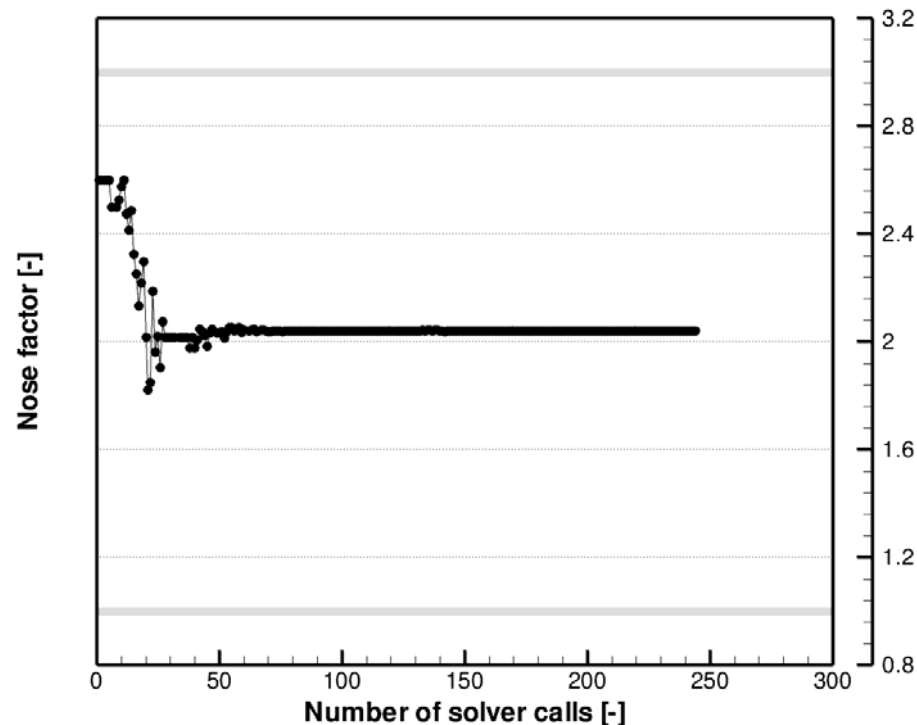
Minimum Drag at 2 Design Points during
Take Off (Maximization of lift to drag ratio)

Design Point 1

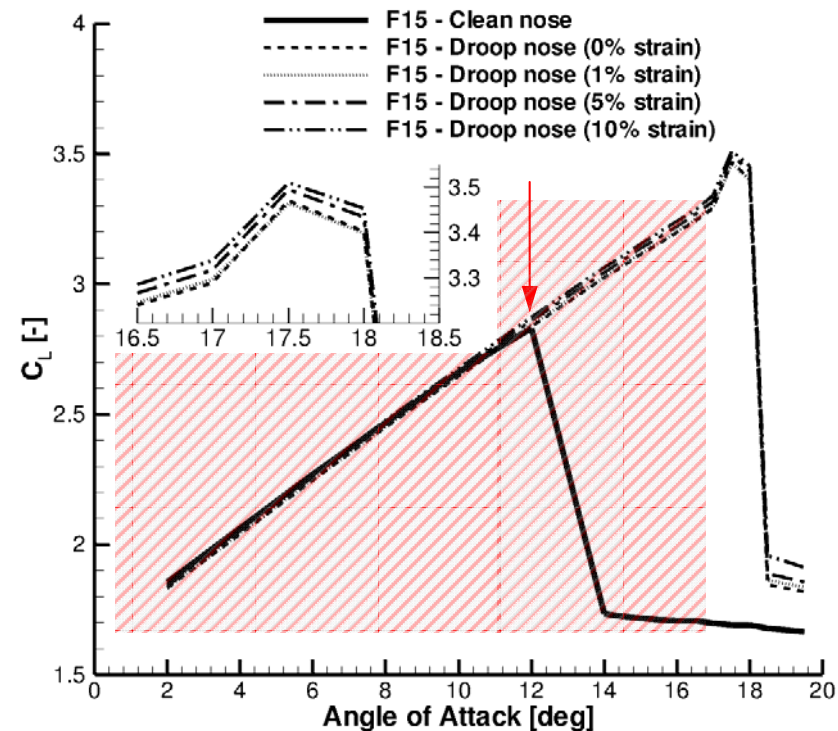
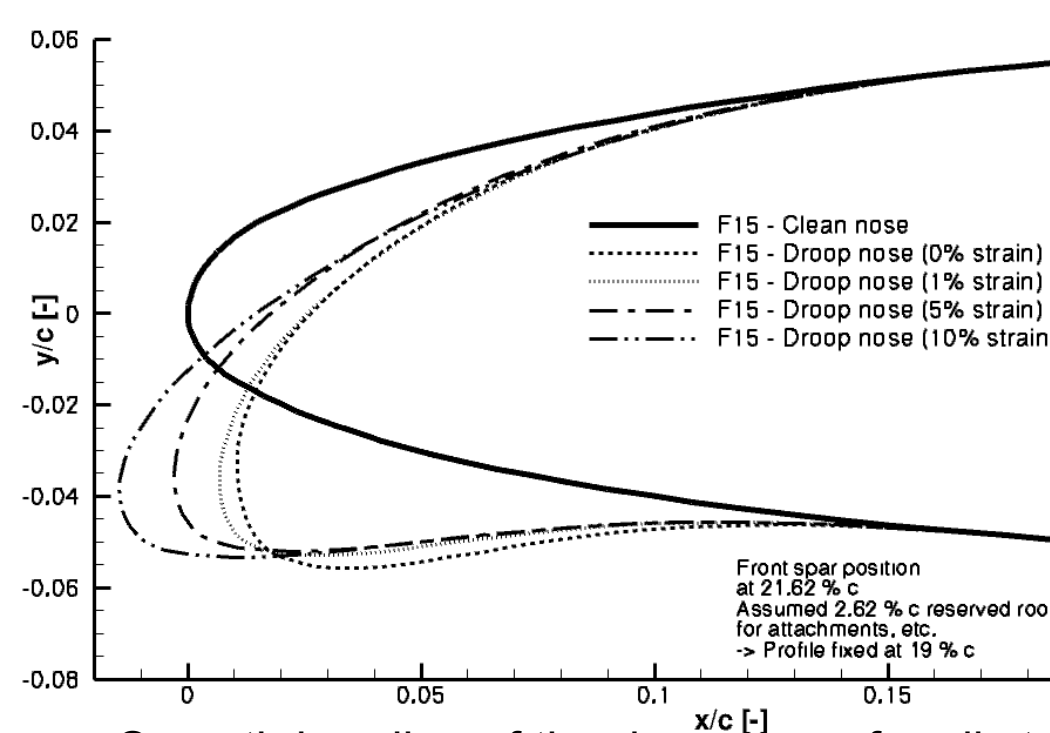
Design Point 2

Results – Convergence Behaviour

- Convergence between 90 and 250 Iterations for the Optimizer
- Convergence is reached for a minimum difference of $1 \cdot 10^{-4}$ of the objective function within the last 10 Iterations

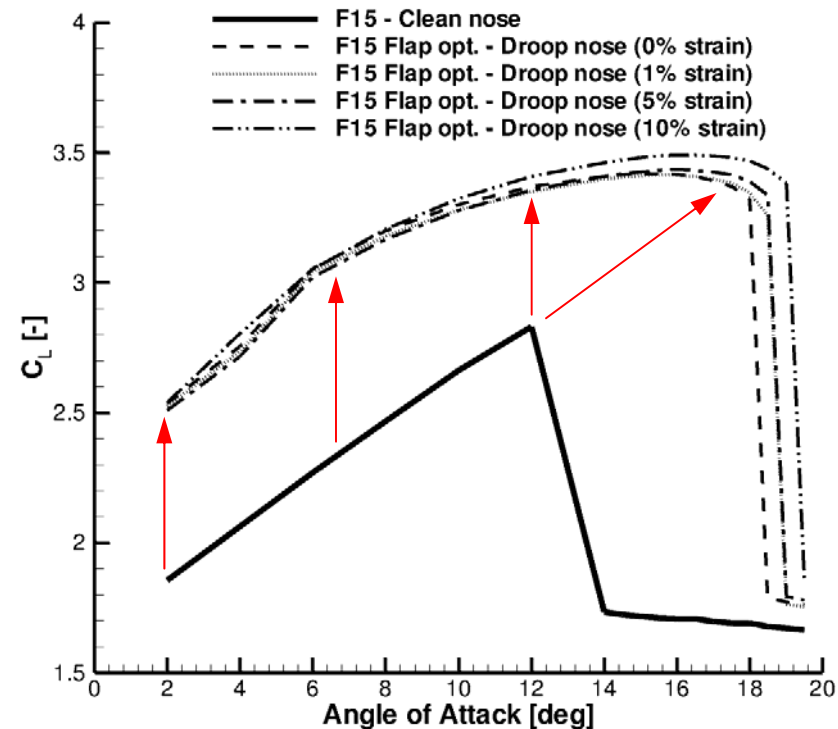
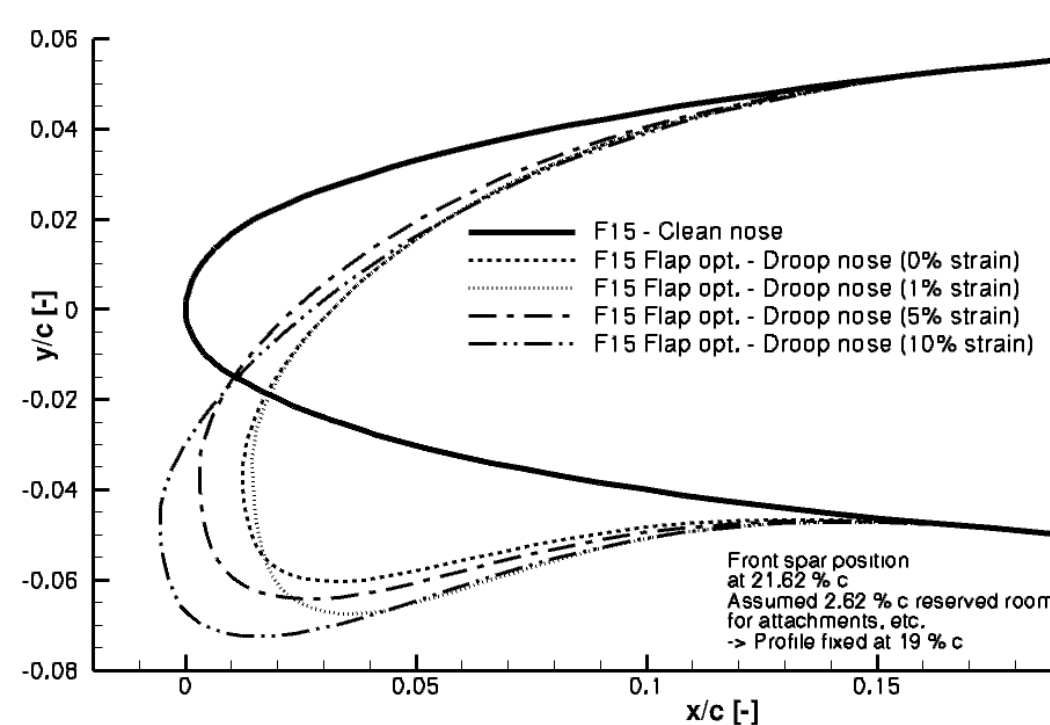


Results – Landing / Without Flap Setting



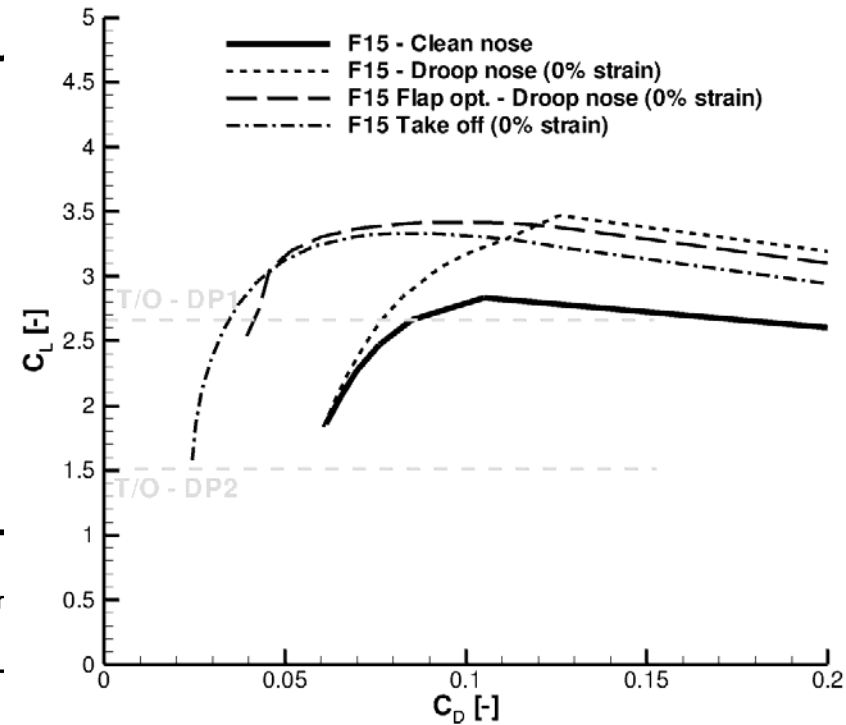
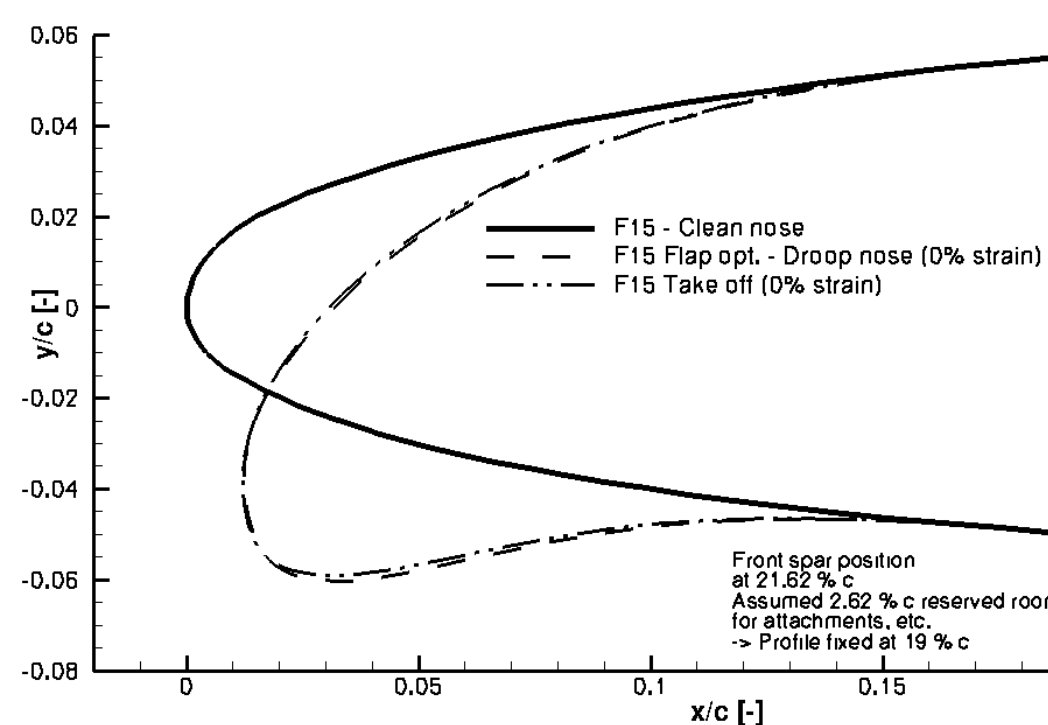
- Smooth bending of the droop nose for all strain rates
- Getting thinner for increasing strain rates (suction peak)
- Droop nose enhances α_{Max} and creates an abrupt wing stall (ill-posed initial flap setting)
- No lift gain for 1% strain; $\Delta C_L = 0.02$ for 5% strain; $\Delta C_L = 0.04$ for 10% strain

Results – Landing / With Flap Setting



- Smaller gap (almost constant with diff. strain rates), larger overlap
- Larger droop of the leading edge compared to the one without flap setting opt.
- Noticeable improvement for lower Angles of Attack (as required in the objective)
- Improvement of $C_{L,Max}$ and α_{Max} for prolongation of the droop nose

Results – TakeOff / With Flap Setting



- Minimization of drag entails a reduction of the flap deployment angle
- Incidentally a similar droop nose shape for the take off setting
- Good high lift performance for all angles of attack, especially lower incidences
- Drag reduction at both design points



Conclusion

- Landing and Take Off settings were numerically optimized for a new smart droop nose high lift device using DLR Megacads, FLOWer and CHAeOPS
- The influence of material strain were investigated via four different strain rates (0, 1, 5, 10% prolongation)
- The Landing optimization is driven by lift optimization
- Keeping the initial flap setting constant leads to an unsatisfying final shape with large areas of separation on the flap independent of the angle of attack
- An inclusion of the flap setting parameters leads to an improved behaviour and a well adapted leading edge droop
- The take off setting is derived in a similar manner reducing drag at two design points
- The leading edge for take off is incidentally congruent to the landing equivalent



Outlook (from an Aerodynamic Point of View)

- Transfer Smart Structures to Laminar Wing Components (also addressed in SADE – HARLS wing)
- Still Room for Improvements for the Methods and Tools - Optimization Algorithms, Higher Order CFD Methods, Formulation of Target Function (addressed in EU project DeSiReH)
- Push Towards Forward Swept Wing Design

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- Surface quality for CFRP materials
 - Laminarity preservation for surface contamination (insect impact)
 - Component integration (engines)
 - ...



Thank you for your attention ...

